

March 1999

# LM2681

# **Switched Capacitor Voltage Converter**

# **General Description**

The LM2681 CMOS charge-pump voltage converter operates as a voltage doubler for an input voltage in the range of +2.5V to +5.5V. Two low cost capacitors and a diode (needed during start-up) is used in this circuit to provide up to 20 mA of output current. The LM2681 can also work as a voltage divider to split a voltage in the range of +1.8V to +11V in half.

The LM2681 operates at 160 kHz oscillator frequency to reduce output resistance and voltage ripple. With an operating current of only 550  $\mu\text{A}$  (operating efficiency greater than 90% with most loads) the LM2681 provides ideal performance for battery powered systems. The device is in SOT-23-6 package.

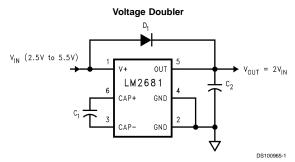
## **Features**

- Doubles or Splits Input Supply Voltage
- SOT23-6 Package
- 15Ω Typical Output Impedance
- 90% Typical Conversion Efficiency at 20 mA

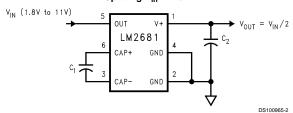
# **Applications**

- Cellular Phones
- Pagers
- PDAs
- Operational Amplifier Power Suppliers
- Interface Power Suppliers
- Handheld Instruments

# **Basic Application Circuits**



## Splitting V<sub>in</sub> in Half



## **Absolute Maximum Ratings** (Note 1)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/Distributors for availability and specifications.

Supply Voltage (V+ to GND, or GND to OUT) 5.8V
V+ and OUT Continuous Output Current 30 mA
Output Short-Circuit Duration to GND (Note 2) 1 sec.

Continuous Power

Dissipation (T<sub>A</sub> = 25°C)(Note 3)

 $\begin{array}{ccc} T_{JMax}(\mbox{Note 3}) & 150\mbox{°C} \\ \theta_{JA} \mbox{ (Note 3)} & 210\mbox{°C/W} \\ \mbox{Operating Junction Temperature} & -40\mbox{° to }85\mbox{°C} \\ \mbox{Range} & \\ \mbox{Storage Temperature Range} & -65\mbox{°C to }+150\mbox{°C} \\ \mbox{Lead Temp. (Soldering, 10 seconds)} & 300\mbox{°C} \\ \end{array}$ 

2kV

## **Electrical Characteristics**

Limits in standard typeface are for  $T_J$  = 25°C, and limits in **boldface** type apply over the full operating temperature range. Unless otherwise specified: V+ = 5V,  $C_1$  =  $C_2$  = 3.3  $\mu$ F. (Note 4)

600 mW

**ESD Rating** 

Symbol	Parameter	Condition	Min	Тур	Max	Units
V+	Supply Voltage	2.5			5.5	V
IQ	Supply Current	No Load 550		1000	μA	
IL	Output Current	20			mA	
R <sub>SW</sub>	Sum of the R <sub>ds(on)</sub> of the four internal MOSFET switches	I <sub>L</sub> = 20 mA	8 16		Ω	
R <sub>OUT</sub>	Output Resistance (Note 5)	I <sub>L</sub> = 20 mA		15	40	Ω
fosc	Oscillator Frequency	(Note 6)	80	160		kHz
f <sub>sw</sub>	Switching Frequency	(Note 6)	40	80		kHz
P <sub>EFF</sub>	Power Efficiency	R <sub>L</sub> (1.0k) between GND and OUT	<b>86</b> 93			%
		I <sub>L</sub> = 20 mA to GND		90		
V <sub>OEFF</sub>	Voltage Conversion Efficiency	No Load	99	99.96		%

Note 1: Absolute maximum ratings indicate limits beyond which damage to the device may occur. Electrical specifications do not apply when operating the device beyond its rated operating conditions.

Note 2: OUT may be shorted to GND for one second without damage. However, shorting OUT to V+ may damage the device and should be avoided. Also, for temperatures above 85°C, OUT must not be shorted to GND or V+, or device may be damaged.

Note 3: The maximum allowable power dissipation is calculated by using  $P_{DMax} = (T_{JMax} - T_A)/\theta_{JA}$ , where  $T_{JMax}$  is the maximum junction temperature,  $T_A$  is the ambient temperature, and  $\theta_{JA}$  is the junction-to-ambient thermal resistance of the specified package.

Note 4: In the test circuit, capacitors  $C_1$  and  $C_2$  are 3.3  $\mu$ F, 0.3 $\Omega$  maximum ESR capacitors. Capacitors with higher ESR will increase output resistance, reduce output voltage and efficiency.

Note 5: Specified output resistance includes internal switch resistance and capacitor ESR. See the details in the application information for positive voltage doubler.

**Note 6:** The output switches operate at one half of the oscillator frequency,  $f_{OSC} = 2f_{SW}$ .

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# **Test Circuit**

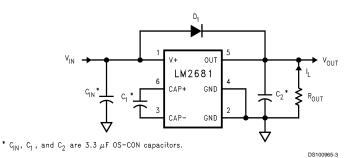
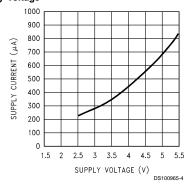


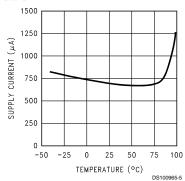
FIGURE 1. LM2681 Test Circuit

# Typical Performance Characteristics (Circuit of Figure 1, V+ = 5V unless otherwise specified)

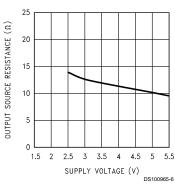
# Supply Current vs Supply Voltage



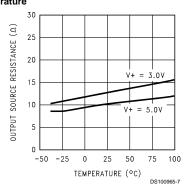
## Supply Current vs Temperature



#### Output Source Resistance vs Supply Voltage



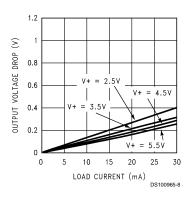
### Output Source Resistance vs Temperature



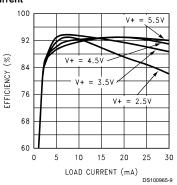
# Typical Performance Characteristics (Circuit of Figure 1, V+ = 5V unless otherwise

specified) (Continued)

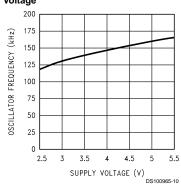
**Output Voltage Drop** vs Load Current



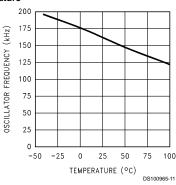
# Efficiency vs Load Current



Oscillator Frequency vs Supply Voltage



Oscillator Frequency vs Temperature



# **Connection Diagram**

6-Lead SOT (M6)





Top View With Package Marking

# **Ordering Information**

Order Number	Package Number	Package Marking	Supplied as	
LM2681M6	MA06A	S10A (Note 7)	Note 7) Tape and Reel (250 units/rail)	
LM2681M6X	MA06A	S10A (Note 7)	Tape and Reel (3000 units/rail)	

Note 7: The first letter "S" identifies the part as a switched capacitor converter. The next two numbers are the device number. The fourth letter "A" indicates the grade. Only one grade is available. Larger quantity reels are available upon request.

Pin	Desc	rin	tion
	<b>D</b> C30	ייי	LIVII

Pin	Name	Function		
		Voltage Doubler	Voltage Split	
1	V+	Power supply positive voltage input	Positive voltage output	
2	GND	Power supply ground input Same as doubler		
3	CAP-	Connect this pin to the negative terminal of the Same as double charge-pump capacitor		
4	GND	Power supply ground input Same as double		
5	OUT	Positive voltage output Power supply positive input		
6	CAP+	Connect this pin to the positive terminal of the charge-pump capacitor	Same as doubler	

# **Circuit Description**

The LM2681 contains four large CMOS switches which are switched in a sequence to double the input supply voltage. Energy transfer and storage are provided by external capacitors. Figure 2 illustrates the voltage conversion scheme. When  $\mathbf{S}_2$  and  $\mathbf{S}_4$  are closed,  $\mathbf{C}_1$  charges to the supply voltage V+. During this time interval, switches  $\mathbf{S}_1$  and  $\mathbf{S}_3$  are open. In the next time interval,  $\mathbf{S}_2$  and  $\mathbf{S}_4$  are open; at the same time,  $\mathbf{S}_1$  and  $\mathbf{S}_3$  are closed, the sum of the input voltage V+ and the voltage across  $\mathbf{C}_1$  gives the 2V+ output voltage when there is no load. The output voltage drop when a load is added is determined by the parasitic resistance ( $\mathbf{R}_{d^-}$  s(on) of the MOSFET switches and the ESR of the capacitors) and the charge transfer loss between capacitors. Details will be discussed in the following application information section.

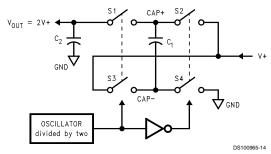


FIGURE 2. Voltage Doubling Principle

# **Application Information**

#### **Positive Voltage Doubler**

The main application of the LM2681 is to double the input voltage. The range of the input supply voltage is 2.5V to 5.5V

The output characteristics of this circuit can be approximated by an ideal voltage source in series with a resistance. The voltage source equals 2V+. The output resistance  $R_{\text{out}}$  is a function of the ON resistance of the internal MOSFET switches, the oscillator frequency, the capacitance and ESR of  $C_1$  and  $C_2$ . Since the switching current charging and discharging  $C_1$  is approximately twice as the output current, the effect of the ESR of the pumping capacitor  $C_1$  will be multiplied by four in the output resistance. The output capacitor  $C_2$  is charging and discharging at a current approximately

equal to the output current, therefore, its ESR only counts once in the output resistance. A good approximation of  $R_{\text{out}}$  is:

$$R_{OUT} \cong 2R_{SW} + \frac{2}{f_{OSC} \times C_1} + 4ESR_{C1} + ESR_{C2}$$

where  $R_{\text{SW}}$  is the sum of the ON resistance of the internal MOSFET switches shown in Figure 2.

The peak-to-peak output voltage ripple is determined by the oscillator frequency, the capacitance and ESR of the output capacitor  $\mathbf{C}_2$ :

$$V_{RIPPLE} = \frac{I_L}{f_{OSC} \times C_2} + 2 \times I_L \times ESR_{C2}$$

High capacitance, low ESR capacitors can reduce both the output reslistance and the voltage ripple.

The Schottky diode  $D_1$  is only needed for start-up. The internal oscillator circuit uses the OUT pin and the GND pin. Voltage across OUT and GND must be larger than 1.8V to insure the operation of the oscillator. During start-up,  $D_1$  is used to charge up the voltage at the OUT pin to start the oscillator; also, it protects the device from turning-on its own parasitic diode and potentially latching-up. Therefore, the Schottky diode  $D_1$  should have enough current carrying capability to charge the output capacitor at start-up, as well as a low forward voltage to prevent the internal parasitic diode from turning-on. A Schottky diode like 1N5817 can be used for most applications. If the input voltage ramp is less than 10V/ms, a smaller Schottky diode like MBR0520LT1 can be used to reduce the circuit size.

## Split V+ in Half

Another interesting application shown in the Basic Application Circuits is using the LM2681 as a precision voltage divider. This circuit can be derived from the voltage doubler by switching the input and output connections. In the voltage divider, the input voltage applies across the OUT pin and the GND pin (which are the power rails for the internal oscillator), therefore no start-up diode is needed. Also, since the off-voltage across each switch equals  $V_{\rm in}/2$ , the input voltage can be raised to +11V.

# Application Information (Continued)

#### **Capacitor Selection**

As discussed in the *Positive Voltage Doubler* section, the output resistance and ripple voltage are dependent on the capacitance and ESR values of the external capacitors. The output voltage drop is the load current times the output resistance, and the power efficiency is

$$\eta = \frac{P_{OUT}}{P_{IN}} = \frac{I_L^2 R_L}{I_L^2 R_L + I_L^2 R_{OUT} + I_Q(V+)}$$

Where  $I_Q(V+)$  is the quiescent power loss of the IC device, and  $I_L{}^2R_{out}$  is the conversion loss associated with the switch on-resistance, the two external capacitors and their ESRs.

The selection of capacitors is based on the specifications of the dropout voltage (which equals  $I_{out}$   $R_{out}$ ), the output voltage ripple, and the converter efficiency. Low ESR capacitors (Table 1) are recommended to maximize efficiency, reduce the output voltage drop and voltage ripple.

# Low ESR Capacitor Manufacturers

Manufacturer	Phone	Capacitor Type
Nichicon Corp.	(708)-843-7500	PL & PF series, through-hole aluminum electrolytic
AVX Corp.	(803)-448-9411	TPS series, surface-mount tantalum
Sprague	(207)-324-4140	593D, 594D, 595D series, surface-mount tantalum
Sanyo	(619)-661-6835	OS-CON series, through-hole aluminum electrolytic
Murata	(800)-831-9172	Ceramic chip capacitors
Taiyo Yuden	(800)-348-2496	Ceramic chip capacitors
Tokin	(408)-432-8020	Ceramic chip capacitors

# Other Applications

### **Paralleling Devices**

Any number of LM2681s can be paralleled to reduce the output resistance. Each device must have its own pumping capacitor  $C_1$ , while only one output capacitor  $C_{\text{out}}$  is needed as shown in Figure 3. The composite output resistance is:

$$R_{OUT} = \frac{R_{OUT} \text{ of each LM2681}}{Number \text{ of Devices}}$$

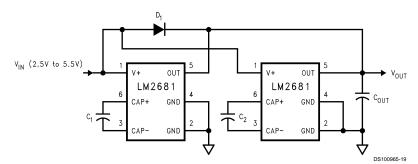


FIGURE 3. Lowering Output Resistance by Paralleling Devices

## **Cascading Devices**

Cascading the LM2681s is an easy way to produce a greater voltage (A two-stage cascade circuit is shown in Figure 4).

The effective output resistance is equal to the weighted sum of each individual device:

$$R_{out} = 1.5R_{out\_1} + R_{out\_2}$$

Note that, the increasing of the number of cascading stages is pracitically limited since it significantly reduces the efficiency, increases the output resistnace and output voltage ripple.

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# Other Applications (Continued)

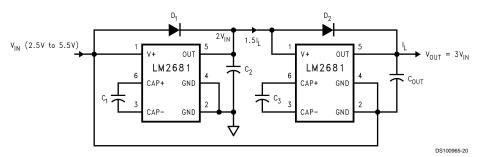


FIGURE 4. Increasing Output Voltage by Cascading Devices

## Regulating $V_{\rm OUT}$

It is possible to regulate the output of the LM2681 by use of a low dropout regulator (such as LP2980-5.0). The whole converter is depicted in Figure 5.

Note that, the following conditions must be satisfied simultaneously for worst case design:

A different output voltage is possible by use of LP2980-3.3, LP2980-3.0, or LP2980-adj.

$$\begin{aligned} &2V_{\text{in\_min}} > V_{\text{out\_min}} + V_{\text{drop\_max}} \text{ (LP2980)} + I_{\text{out\_max}} \text{ x } R_{\text{out\_max}} \text{ (LM2681)} \\ &2V_{\text{in\_max}} < V_{\text{out\_max}} + V_{\text{drop\_min}} \text{ (LP2980)} + I_{\text{out\_min}} \text{ x } R_{\text{out\_min}} \text{ (LM2681)} \end{aligned}$$

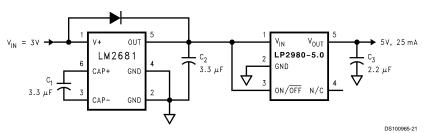
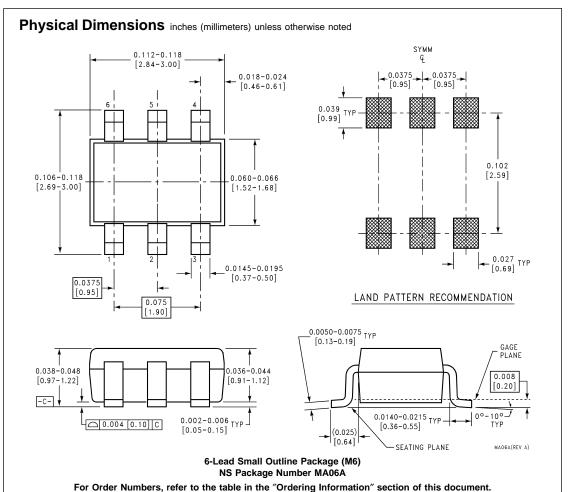


FIGURE 5. Generate a Regulated +5V from +3V Input Voltage



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